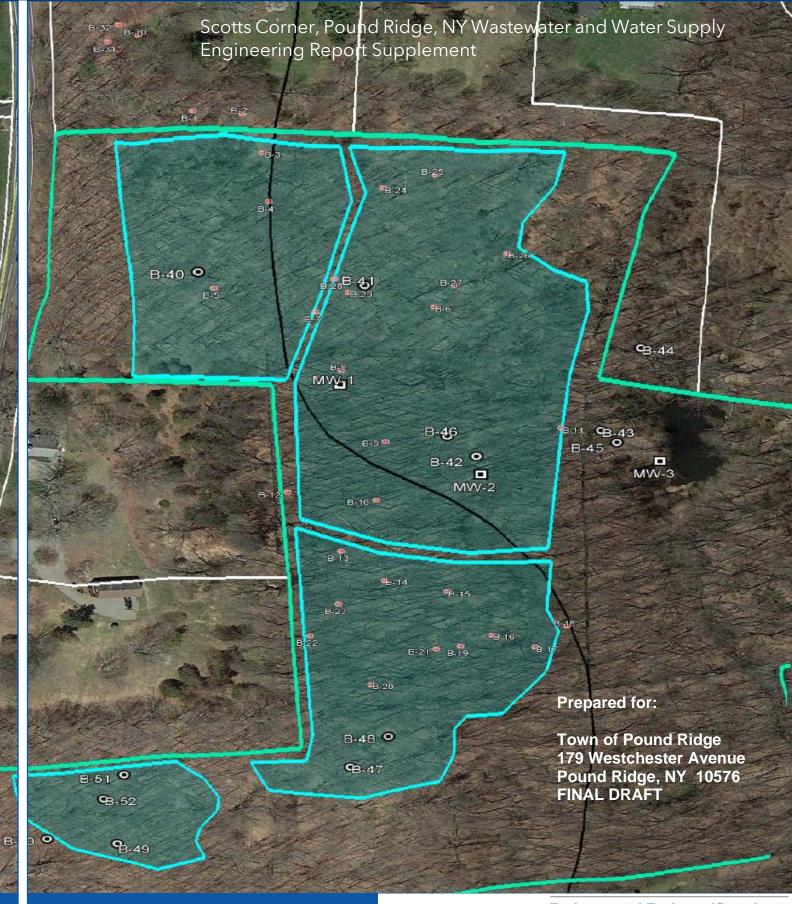
a. Old Pound Parcels – Evaluation for Effluent Disposal

Old Pound Road Parcels - Evaluation for Effluent Disposal



Environmental Engineers/Consultants

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ENGINEERING REPORT CERTIFICATION

During the preparation of this Engineering Report Supplement, I have studied and evaluated the cost and effectiveness of the processes, materials, techniques, and technologies for carrying out the proposed project or activity for which assistance is being sought from the New York State Clean Water State Revolving Fund. In my professional opinion, I have recommended for selection, to the maximum extent practicable, a project or activity that maximizes the potential for efficient water use, reuse, recapture, and conservation, and energy conservation, taking into account the cost of constructing the project or activity, the cost of operating and maintaining the project or activity over the life of the project or activity, and the cost of replacing the project and activity.

This Engineering Report Supplement has been prepared in accordance with the NYSDEC New York State Design Standards for Intermediate Sized Wastewater Treatment Systems dated March 5, 2014 https://www.dec.ny.gov/docs/water_pdf/2014designstd.pdf

Title of Engineering Report: Scotts Corner, Pound Ridge, NY Wastewater and

Water Supply Engineering Report Supplement

Date of Report Supplement: November 16, 2020

Professional Engineer's Name: Pio S. Lombardo, P.E., NYS PE # 056900

Signature:

Date: November 16, 2020

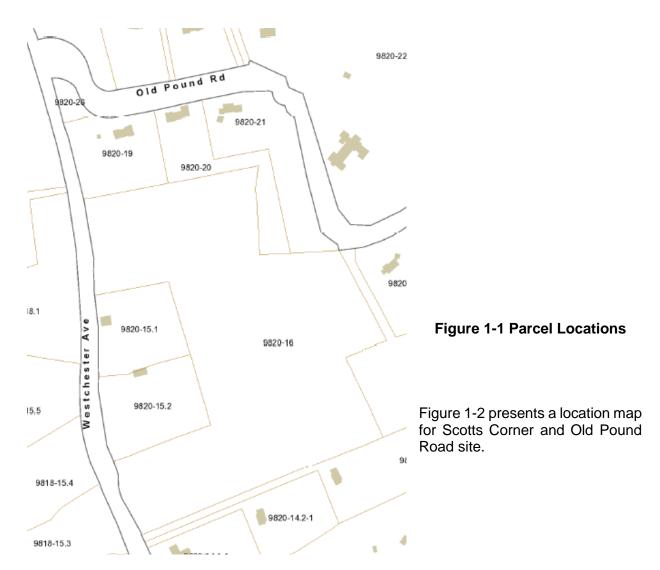


1 INTRODUCTION

This Report provides draft interim findings associated with the following activities that were authorized by the October 6, 2020 Agreement between the Town of Pound Ridge and Lombardo Associates, Inc. (LAI).

- 1. 2 3 days of borings at Old Pound Road site using a direct push machine and manually approximate location.
- 2. Create 3-D representation of subsurface depth to rock, groundwater and soil types.
- 3. Collect a minimum of ten (10) soil samples and have sieve analysis performed to estimate hydraulic conductivity.
- Estimate disposal capacity with consideration of setbacks from property lines and water bodies/wetlands.
- 5. Brief Report on findings

During summer 2020, the Town purchased parcels 9820-16, 9820-19 and 9820-26 with sizes of 18.86 acres, 2.23 acres and 0.25 acres, respectively. Figure 1-1 illustrates the parcels locations.



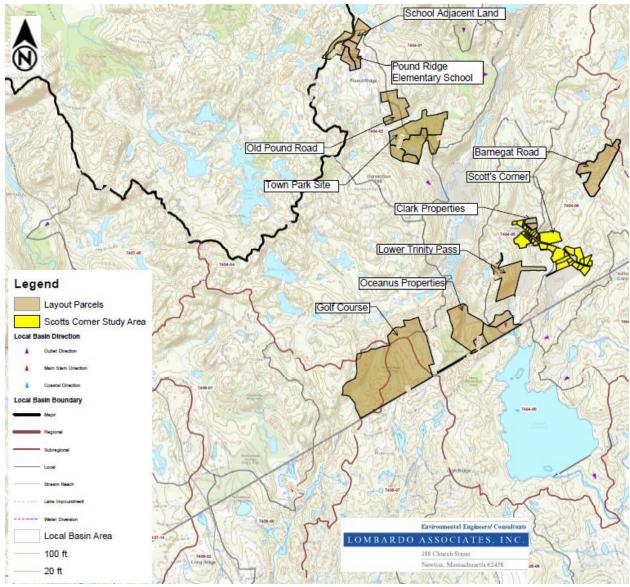


Figure 1-2 Scotts Corner - Old Pound Road - Location Map

With consideration of appropriate separations to property lines and wetlands and avoidance of steep sloped areas (hereinafter referred to as "available area"), Figure 1-3 presents preliminary available area for locating treatment and / or disposal at Old Pound Road site.



Figure 1-3 Old Pound Road – Available Area Map

Most of the site's available area was disaggregated into zones based upon topography considerations, as shown on Figure 1-4. Approximate zone areas:

- 1 73,000-sq. ft
- 2 151,000-sq. ft
- 3 92,000-sq. ft
- 4 31,000-sq. ft

for total of, say, 350,000 +/- sf.

For preliminary design purposes, wastewater treatment and disposal demands are 40,000 gpd for existing uses and up to 80,000 gpd for build out uses.

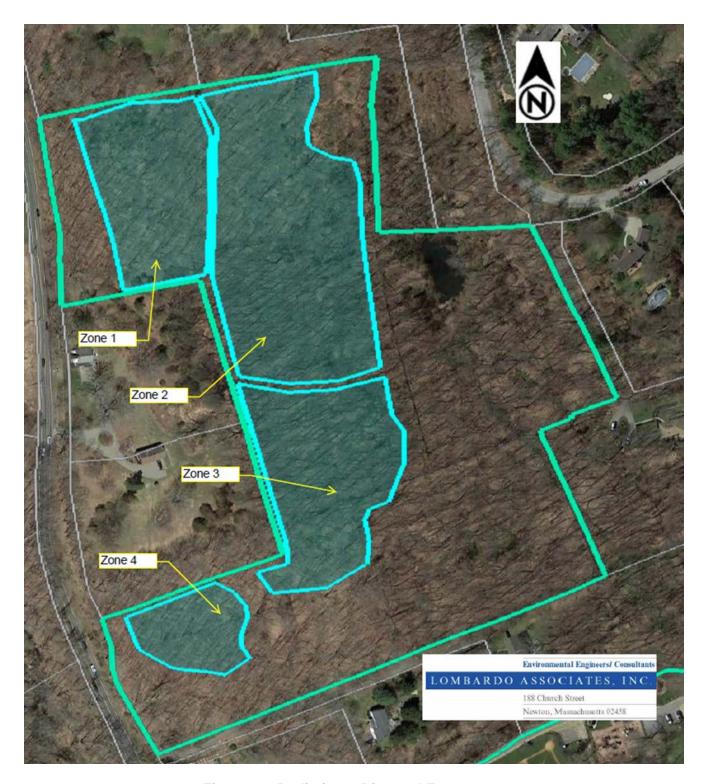


Figure 1-4 Preliminary Disposal Zones

2 BORINGS - LOCATIONS & SOIL PROFILES

Figure 2-1 illustrates the approximate location of the 44 soil borings to bedrock taken on the property. As location information was obtained by a cell phone app and cell reception was poor in some areas, the location data needs to be viewed with caution, especially borings 40 - 52.

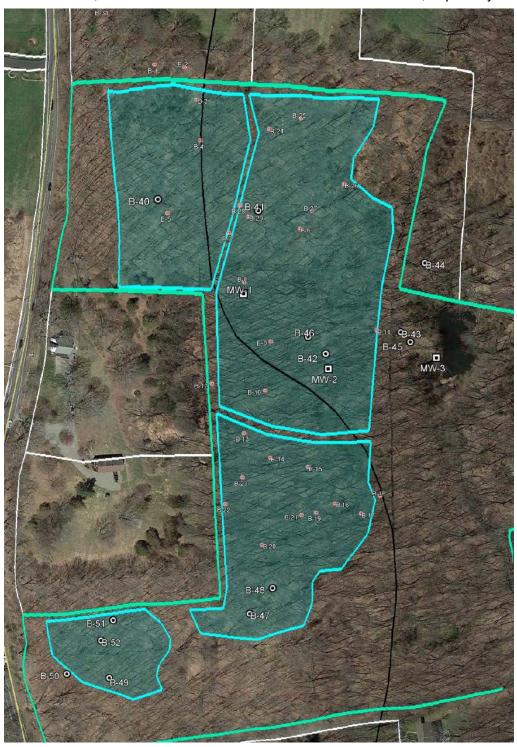


Table 2-1 presents depth to bedrock for the 44 locations with an average of 10 feet below (bg). grade The soil profiles surficial geology of the 44 soil borings are presented on Table 2-2. The data indicates that the surficial geology typically a fine sand.

Table 2-3 presents sieve analysis results for 11 samples taken at borings 4, 7, 13 & 21.

Figure 2-1 Borings Location Map

Table 2-1 Depth to Bedrock at Boring Locations

Boring #	Depth to Bedrock (feet)	Boring #	Depth to Bedrock (feet)
1	12	53	10
2	8	54	9
3	9	55	8
4	10	56	8
5	12	57	10
6	10	58	5
7	15	59	10
8	10	60	10
9	7.5	61	15
10	7.5	40	15
11	10	41	10
12	13	42	10
13	13	43	10
14	8	44	10
15	10	45	14
16	9	46	11
17	5	47	7
18	3	48	10
19	10	49	10
20	10	50	12
21	14	51	9
22	8	52	12.5

Table 2-2 Soil Profiles

												abi	e z-	2 50	III Pro	ofiles	5									
									Soil	Bori	ngs @	olo 🤋	Pou	nd Ro	ad Site	e										
Boring # / Soil Depth (ft)	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	Boring # / Soil Depth (ft)		
0.5																								0.5	Тор	soil
1																								1	clay	ey sand
1.5																								1.5	silt	ysand
2																								2		sand
3																								3		ie sand h coarse
4																								4		sand
5																								5		e sand
6																								6	with	h gravel
7																								7		
8																								8		
9																								9		
10																								10		
11																								11		
12																								12		
13																								13		
14																								14		
15																								15		
Depth to Bedrock (feet)	12	8	9	10	12	10	15	10	7.5	7.5	10	13	13	8	10	9	5	3	10	10	14	8	10			
Groundwa	teror	28 0	ct 202	202									no	ne ob	served	t										
								MW-1								white										

Boring # / Soil Depth (ft)	24	25	26	27	28	29	30	31	40	41	42	43	44	45	46	47	48	49	50	51	52	Boring #/Soil Depth (ft)	
0.5																						0.5	Topsoil
1																						1	clayey sand
1.5																						1.5	siltysand
2																						2	fine sand
3																						3	fine sand with coarse
4																						4	sand
5																						5	fine sand
6																						6	with gravel
7																						7	
8																						8	
9																						9	
10																						10	
11																						11	
12																						12	
13																					12.5	13	
14																						14	
15																						15	
Depth to Bedrock (feet)	9	8	8	10	5	10	10	15	15	10	10	10	10	14	11	7	10	10	12	9	12.5		
GW on 11-9-20							No G	W						5.5' bg			N	o GW	/				
														MW-3	MW-2								
															MW-2 h	nas conti	inuous	GW el	evatio	n mon	itor		

Table 2-3 Soil Sieve Analysis & Hydraulic Conductivity Calculations

				lysis - 7 (Hydra		uctivity (ft/	/day)
Count	Boring #	Feet below ground	% Gravel	% Sand	% Silt	% Clay	uniformity coefficient (C _u)**	D ₁₀ (mm)	At Boring	Shallow Elev.	Mid Elev	Deep Soils Elev
1	4	4	60.1	30.4	8.4	1.1	192	0.0795	17.9	17.9		
2	4	7	33.8	40.7	22.7	2.8	58	0.0412	4.8		4.8	
3	7	2	5.8	55.3	34.9	4	6	0.0394	4.4	4.4		
4	7	8	27.7	55.4	14.7	2.2	41	0.0524	7.8		7.8	
5	7	12	35.1	51.5	11.7	1.7	62	0.0598	10.1			10.1
6	13	3	43.3	43.9	11.2	1.6	104	0.0621	10.9	10.9		
7	13	9	38.2	48	12.6	1.2	71	0.0602	10.3		10.3	
8	13	12	17.4	61.1	19.7	1.8	13	0.0487	6.7			6.7
9	21	3	30	47.5	20.2	2.3	29	0.0455	5.9			
10	21	9	50.8	36.1	11.6	1.5	203	0.0604	10.3		10.3	
11	21	13	18.6	52.9	25.3	3.2	10	0.0408	4.7			4.7
* Hydra	ulic Cond	ductivity ca	lculated	with Haze	en-Williar	ns formu	а		Average	11.1	8.3	7.2
**Soils	with C _u	<= 4 are co	nsidered	l to be "po	orly grad	ed" or un	iform		Average of	Mid & De	ер	7.82
$C_u = (D_u)$	₆₀ /D ₁₀)								Geomean	of Mid & D	eep	7.45

3 BEDROCK CONTOURS & GROUDWATER FLOW ISSUES

Figure 3-1 presents computer generated bedrock elevation contours based upon the Table 2-1 depth to rock data and 2-foot surface topographic information obtained from 2020 Westchester County GIS. LAI created a computer generated 1-foot topographic map.

Estimated groundwater flow path based upon surface topography is presented on Figure 3-2.

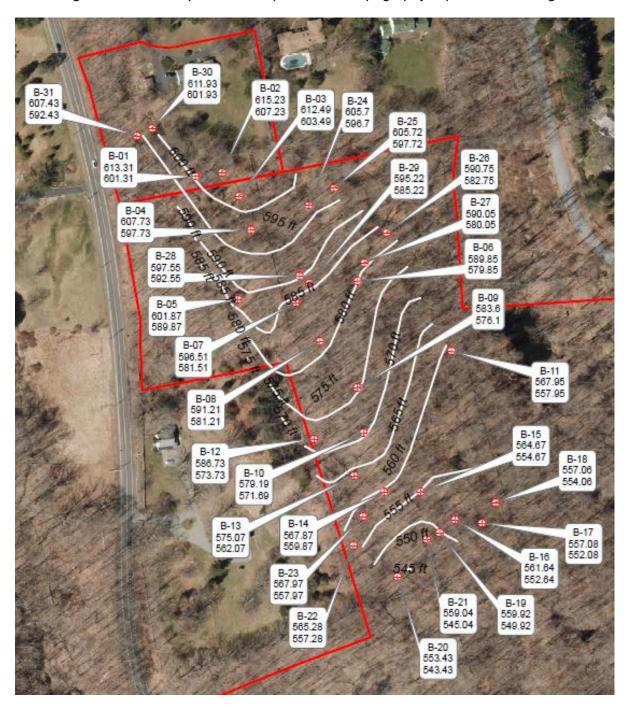


Figure 3-1 Preliminary Bedrock Contours

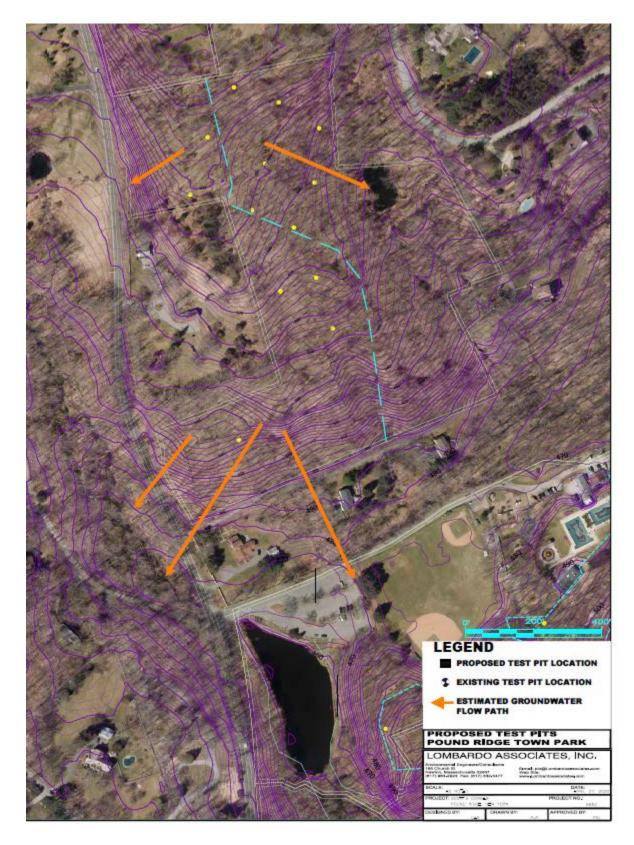


Figure 3-2 Preliminary GW Flow Direction

4 ESTIMATE DISPOSAL CAPACITY

Disposal capacity of final layouts will be determined by use of the USGS Groundwater Flow computer model MODFLOW. For analytical purposes only, Darcy's Law capacity estimates are prepared to provide preliminary insights to the disposal capacities of the candidate sites.

Darcy's Law Capacity Estimates Methodology

The treated wastewater disposal capacity is estimated in the following manner:

- 1. Available Area determined as discussed in Section 1
- 2. Viable zones within the available area were identified based upon surface and bedrock topography (work with contours) and preliminary disposal system layout considerations.
- 3. Darcy's Law disposal capacity of the drainfield zones was calculated at the downgradient face of the zone as follows, see Figures 4-1.
- 4. $Q = K^*A^*i$, where Q = volumetric flow (cf/day),

K = Hydraulic conductivity (ft/day) of unsaturated zone,

A = cross sectional area (sf) of discharge cross sectional area

i = groundwater slope

- 5.
- i. Hydraulic conductivity (K) of soils estimated based upon sieve analysis and use of Hazen Williams formula K= C* (D10)2, where K = Hydraulic conductivity (cm/sec), D10 = 10th percentile grain size by weight in mm, C = dimensionless coefficient =1, for K in cm/sec and D10 in mm.;
- ii. Borings data basis depth to bedrock,
- iii. No mottling basis for no significant seasonal high groundwater elevation
- iv. Cross Sectional area computed by:
 - ✓ Length measured as the furthest downgradient face of zone See Figure 4-2 for initial layouts
 - ✓ Depth calculated by subtracting from depth to GW/BR (ii above)
 - separation between grade and bottom of drip disposal system;
 - separation between drip bottom and max mounded GW elev.
- 6. Darcy's Law flow estimates calculated

Table 4-1 presents estimated site disposal capacity using Darcy's Law.

The lack of soil mottling suggest that groundwater buildup does not occur at the site. Three groundwater monitoring wells were installed as shown on Figure 2-1 and Table 2-2. Groundwater was observed at MW-3, whose elevation appears to be governed by Pond elevation, which in turn is governed by an outlet weir elevation.



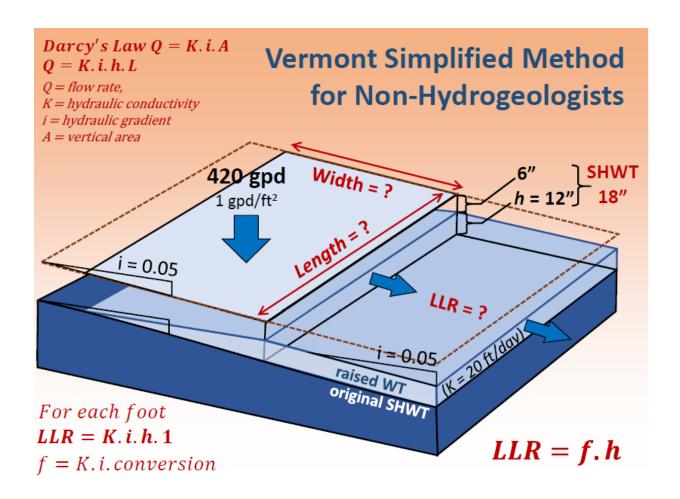


Figure 4-1 Simplified Darcy's Law Mounding Analysis-Example

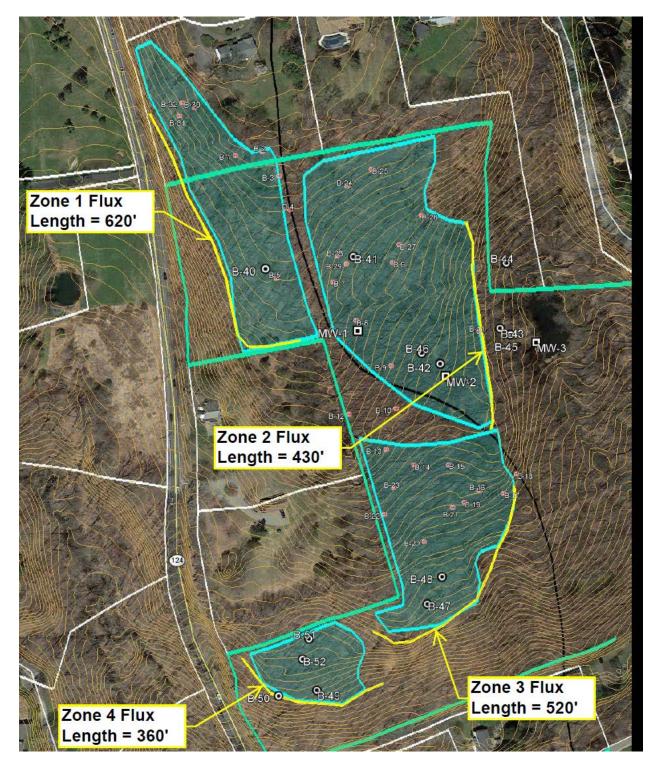


Figure 4-2 Preliminary Estimates of groundwater zone faces

Table 4-1 Disposal Capacity Estimates with Varying GW & Separation Elevations

		Ol	d Pound	Road Po	otential	Drainfield 2	Zones Capaci	ty Analysi	is - No Gr	oundw	ater		
DF	GW		GW Depth	Depth	Depth	Disp. Sys.	Min. Separation	Max.	Hyd.		Flux	Flow	- Darcy
Zone #	Flux Length (ft)	Soil Type	Above Bed rock	to BR (ft)	to GW (ft)	Depth Below Grade (ft)	Between Drip & GW Mound (ft)	Mound Height (ft)	Cond. ⁽¹⁾ (ft/d)	Slope (%)	Area (ft²)	(ft ³ / day)	(gpd)
1	620	ChB	0.00	10.0	10.0	1.0	2.0	7.0	7.8	7.0%	4,340	2,370	17,725
2	430	ChB	0.00	10.0	10.0	1.0	2.0	7.0	7.8	8.0%	3,010	1,878	14,049
3	520	ChC, ChD	0.00	10.0	10.0	1.0	2.0	7.0	7.8	8.0%	3,640	2,271	16,990
4	360	ChD, ChC	0.00	10.0	10.00	1.0	2.0	7.0	7.8	7.0%	2,520	1,376	10,292
(1) From	Sieve An	alysis Ta	ble 2-3. Fo	or referen	ce, averag	e aalue from	Table 17, Westo	hester Coun	ty Soils Sur	vey= 6.6	feet/day	Total	59,056

	Old	Pound	Road Po	tential D	rainfiel	d Zones Ca _l	pacity Analys	is - Groun	dwater 1	foot ak	ove Be	drock	
DF	GW		GW Depth	Depth	Depth	Disp. Sys.	Min. Separation	Max.	Hyd.		Flux	Flow	- Darcy
Zone #	Flux Length (ft)	Soil Type	Above Bed rock	to BR (ft)	to GW (ft)	Depth Below Grade (ft)	Between Drip & GW	Mound Height (ft)	Cond. ⁽¹⁾ (ft/d)	Slope (%)	Area (ft²)	(ft³/ day)	(gpd)
1	620	ChB	1.00	10.0	9.0	1.0	2.0	6.0	7.8	7.0%	3,720	2,031	15,193
2	430	ChB	1.00	10.0	9.0	1.0	2.0	6.0	7.8	8.0%	2,580	1,610	12,042
3	520	ChC, ChD	1.00	10.0	9.0	1.0	2.0	6.0	7.8	8.0%	3,120	1,947	14,563
4	360	ChD, ChC	1.00	10.0	9.00	1.0	2.0	6.0	7.8	7.0%	2,160	1,179	8,822
(1) Fron	ı Sieve An	alvsis Ta	hle 2-3. Fi	or referen	ce. averaa	e galue from	Table 17. Westo	hester Coun	tv Soils Sur	vev= 6.6	feet/day	Total	50.619

	Old I	Pound I	Road Pot	tential D	rainfiel	d Zones Ca _l	pacity Analys	is - Grour	dwater 2	feet ak	ove Be	drock	
DF	GW		GW Depth	Depth	Depth	Disp. Sys.	Min. Separation	Max.	Hyd.		Flux	Flow	- Darcy
Zone #	Flux Length (ft)	Soil Type	Above Bed rock	to BR (ft)	to GW (ft)	Depth Below Grade (ft)	Between Drip & GW Mound (ft)	Mound Height (ft)	Cond. ⁽¹⁾ (ft/d)	Slope (%)	Area (ft²)	(ft³/ day)	(gpd)
1	620	ChB	2.00	10.0	8.0	1.0	2.0	5.0	7.8	7.0%	3,100	1,693	12,661
2	430	ChB	2.00	10.0	8.0	1.0	2.0	5.0	7.8	8.0%	2,150	1,342	10,035
3	520	ChC, ChD	2.00	10.0	8.0	1.0	2.0	5.0	7.8	8.0%	2,600	1,622	12,136
4	360	ChD, ChC	2.00	10.0	8.00	1.0	2.0	5.0	7.8	7.0%	1,800	983	7,351
(1) From	Sieve And	alysis Ta	ble 2-3. Fo	or referen	ce, averag	e aalue from	Table 17, Westo	hester Coun	ty Soils Sur	vey= 6.6	feet/day	Total	42,183

	(Old Pour	nd Road	l Potenti	al Drain	field Zor	nes Capacit	y Analysis - G	roundwa	ter 2 fee	t above	Bedroc	k	
DF		GW		GW Depth	Depth	Depth	Disp. Sys.	Min. Separation	Max.	Hyd.		Flux	Flow	- Darcy
Zone #	Area (sf)	Flux Length (ft)	Soil Type	Above Bed rock	to BR (ft)	to GW (ft)	Depth Below Grade (ft)	Between Drip & GW Mound (ft)	Mound Height (ft)	Cond. ⁽¹⁾ (ft/d)	Slope (%)	Area (ft²)	(ft³/ day)	(gpd)
1	73,000	620	ChB	0.00	10.0	10.0	1.0	1.0	8.0	7.8	7.0%	4,960	2,708	20,257
2	151,000	430	ChB	0.00	10.0	10.0	1.0	1.0	8.0	7.8	8.0%	3,440	2,147	16,056
3	92,000	520	ChC, ChD	0.00	10.0	10.0	1.0	1.0	8.0	7.8	8.0%	4,160	2,596	19,417
4	31,000	360	ChD, ChC	0.00	10.0	10.00	1.0	1.0	8.0	7.8	7.0%	2,880	1,572	11,762
	347,000												Total	67,492

Old Pound Road Potential Drainfie	ld Zones (Capacity A	nalysis Su	mmary
Depth to Bedrock (ft)	10	10	10	10
GW Depth above bedrock (ft)	0	0	1	2
Drip Separation to Mounded GW (ft)	1	2	2	2
Estimated Capacity (gpd)	67,492	59,056	50,619	42,183

It is noted at 80,000 gpd code design flow, average flow is expected to be 40,000 gpd. Consequently, provided that groundwater does not exceed 2 feet above bedrock and groundwater flow patterns from additional data/analysis are consistent with the estimates in this Report, it is Lombardo Associates, Inc.'s opinion that the Old Pound Site has sufficient disposal capacity for the proposed Scotts Corner 80,000 gpd wastewater system. Exact layout and loading of the drip disposal system is a design issue that would be addressed during design process, which occurs after Sewer District formation and bonding.

Pending NYSDEC and WCDoH review, a MODFLOW analysis of the site's capacity may be required for NYSDEC/WCDoH acceptance. To eliminate uncertainties, LAI recommends such an analysis after groundwater elevation data is collected in March – April 2021. In addition to site capacity confirmation, the MODFLOW analysis is used for disposal system design and operation.